

11 Oct 1883

Proposed Bridge over River Glen at Surfleet

Memo of Loads & Strains &c

The bridge is to be 90.0' span centre to centre of bearings with a clear width of 21.0' between handrails; Skew 8.2' no overhead bracing permitted.

Dead load, 90^{lbs} per foot super, for 9" thick of concrete & macadam.

Live load, Two traction engines of 20 tons weight each passing each other at any part of the bridge, together with a crowd load of 3/4^{cut} per foot super on all parts of the bridge not occupied by the traction engines, & a side wind pressure of 40^{lbs} per foot super.

Unit strains, allowed for under such loading are as follows

Main girders; top booms,	3 1/2	tons	per square inch of gross section
" bottom "	5	"	" " net "
" struts	2 1/2	"	" " gross "
" ties	5	"	" " net "
Cross girders; top flange	4	"	" " gross "
" bottom "	5	"	" " net "
Longitudinals; top flange	4 1/2	"	" " gross "
" bottom "	4 1/2	"	" " net "
Shearing on webs	3	"	" " gross "

The type of bridge adopted is with 2 Main girders of Braced Bowstring in form, with vertical struts; working depth 8th of span, top boom curved to an ellipse; Plate cross girders 2.0' deep, placed 8.2' apart suspended to Main girders, & carried out beyond Main girders at intervals, with raking struts up to top boom; Longitudinals of rolled joist iron 4.3' apart; and decking of W.I. arched plates;

Maximum loads upon each bay of 8.2' in length of each main girder under these conditions will be as follows.

<u>Dead load</u> , by concrete & macadam 8.2' x 10.6' x 90 ^{lbs} =	69	cut
add for floor plates 3/8" thick, 8.2' x 11.0' x 15 ^{lbs} =	12	
" " longitudinal, 2/8.2' x bay 35 ^{lbs} =	5	
" " railing & gravel plate, 8.2' x 1/2 ^{cut} =	4	
" " cross girder & bracing, say	14	
" " main girder "	36	
	<u>140</u>	= <u>7 tons</u>

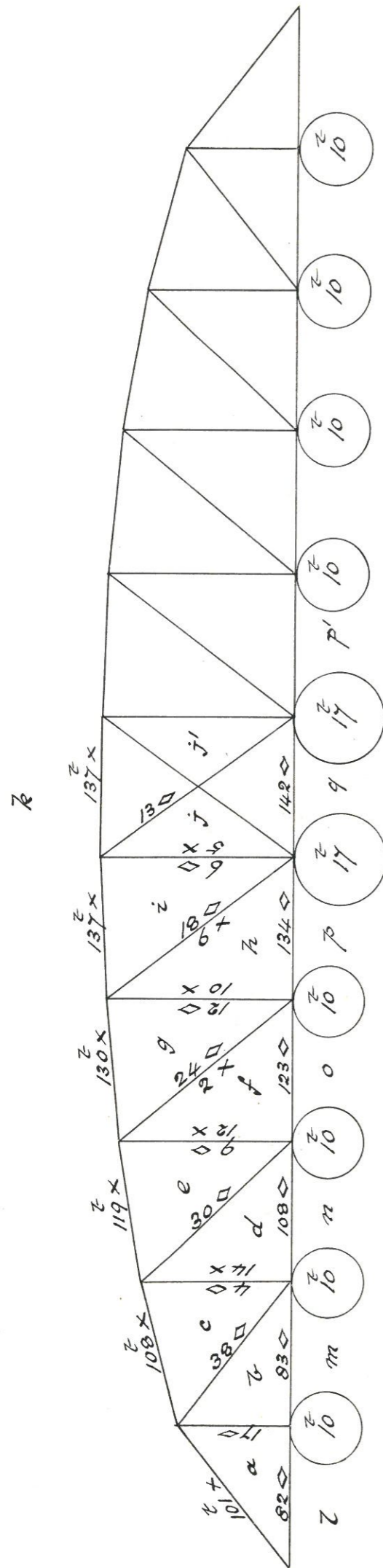
Rolling Load, by two 20^{ton} traction engines passing, each cross girder is taken as transmitting half the weight of one engine to each main girder = 10 tons

Crowd Load taken upon cross girders not occupied by the engines. 8.2' x 10.6' x 3/4^{cut} = 3 tons

The maximum loads will therefore be 7 + 10 = 17 tons upon any 2 contiguous cross girders; and 7 + 3 = 10 tons on others.

Wind pressure, in consideration of the open character of the main girders & the small obstruction they oppose to the wind it will be sufficient to allow a vertical resisting surface of 6.0' in height for structure & traffic.
90.0' x 6.0' x 40^{lbs} = say 10 tons dist. over girder

The maximum strains upon the various members of main girders by these loads is shown upon the following diagram:

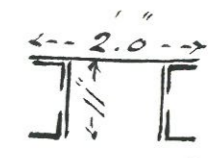


N.B. X denotes Compression
 O denotes Tension

Areas & Sections of Main girders

Top boom

a.k. $101 \div 3\frac{1}{2} = 28.8$ required area
 c.k. $108 \div " = 30.8$ " " }



Section, 1 plate $24 \times \frac{3}{8} = 9$
 2 bars $11 \times \frac{1}{2} = 11$
 4 angles $3 \times 3 \times \frac{1}{2} = 11$ } 31 sq. ins.

e.k. $119 \div 3\frac{1}{2} = 34$ required area; Section 1 plate $24 \times \frac{1}{2} = 12$
 2 bars $11 \times \frac{1}{2} = 11$
 4 Angles $3 \times 3 \times \frac{1}{2} = 11$ } 34 sq. ins.

g.k. $130 \div 3\frac{1}{2} = 37$ required area; Section 1 plate $24 \times \frac{5}{8} = 15$
 2 bars $11 \times \frac{1}{2} = 11$
 4 Angles $3 \times 3 \times \frac{1}{2} = 11$ } 37 sq. ins.

i.k. $137 \div 3\frac{1}{2} = 39$ required area; Section 1 plate $24 \times \frac{3}{4} = 18$
 2 bars $11 \times \frac{1}{2} = 11$
 4 Angles $3 \times 3 \times \frac{1}{2} = 11$ } 40 sq. ins.

Bottom boom

a.u. $82 \div 5 = 16.4$ required area; Section 4 Angles $4 \times 3 \times \frac{1}{2} = 11$
 2 bars $8 \times \frac{1}{2} = 6$ } 17 net sq. ins.

d.u. $108 \div 5 = 21.6$ required area; Section 4 Angles $4 \times 3 \times \frac{1}{2} = 11$
 2 bars $8 \times \frac{1}{2} = 6$
 2 " $8 \times \frac{5}{8} = 7\frac{1}{2}$ } 24\frac{1}{2} sq. ins.

k.p. $134 \div 5 = 26.8$ required area; Section 4 Angles $4 \times 3 \times \frac{1}{2} = 11$
 2 bars $8 \times \frac{1}{2} = 6$
 2 " $8 \times \frac{5}{8} = 7\frac{1}{2}$
 2 " $8 \times \frac{3}{8} = 4\frac{1}{2}$ } 29 sq. ins.

Vertical struts

c.d. $14 \div 2\frac{1}{2} = 5.6$ required area; Section 2 Tees $6 \times 3 \times \frac{1}{2} = 8\frac{1}{2}$ sq. ins.

Diagonal ties

b.c. $38 \div 5 = 7.6$ required area; Section 2 Angles $4 \times 4 \times \frac{5}{8} = 7.8$ net sq. ins.

d.e. 30 " " " " 2 " $4 \times 4 \times \frac{1}{2} = 6.5$ "

f.g. 24 " " " " 2 " $4 \times 3 \times \frac{1}{2} = 5.5$ "

h.i. 18 " " " " 2 " $4 \times 3 \times \frac{3}{8} = 4.1$ "

j.j' 13 " " " " 2 bars $11 \times \frac{1}{2} = 2.2$ "

Cross girder

made 2'0" deep over web; working depth = 1'10"
 " length = 23'3"

Max. load with one pair of wheels from each engine.

Road metal & floor plates $21.0 \times 8.0 \times 1 = 8\frac{1}{2}$ tons

add for longitudinals say $\frac{1}{2}$ "

" " own weight " 1 "

rolling load 20 "

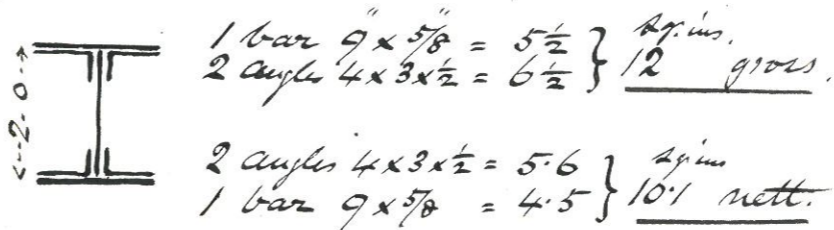
30 tons distributed

Strain on flanges at centre $\frac{30 \times 23\frac{3}{4}}{8 \times 1.83} = 48$ tons

Top flange $48 \div 4 = 12$ sq ins required area

bottom " $48 \div 5 = 9.6$ " " "

Section



Longitudinal girder

made of rolled joist 10" deep, working depth = 9"
 " length = 7'6"

Max. load with one wheel of engine at centre.

Road metal & floor plates $7.6 \times 4.3 \times 1 = 33$ } tons

add own weight say 2 } $1\frac{3}{4}$ distributed

Rolling load 5 tons at centre = 10 "

$11\frac{3}{4}$ "

(say 12 tons)

Strain on flanges at centre $\frac{12 \times 7\frac{1}{2}}{8 \times \frac{3}{4}} = 15$ tons

$15 \div 4\frac{1}{2} = 3\frac{1}{3}$ sq ins required areas

Section I 10 x 5 x 35 joist with flange area of 3.6 sq ins

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